

# Two-Dimensional Antenna Beamsteering Using Metamaterial Transmitarray

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**Abstract:** A novel 2D-beamsteering technique employing a metamaterial transmitarray is presented. The proposed transmitarray, when coupled to a conventional horn antenna, allows its original radiation pattern to be steered in both elevation and azimuth planes. A fixed 25° steering in  $\theta$  and  $\phi$  (spherical coordinates) was achieved through electromagnetic simulations and validated against experimental results, obtained from a prototype comprised of 5 x 5 unit-cells at 5.35 GHz, carried out inside an anechoic chamber.

**Keywords:** Beamsteering, metamaterials, transmitarray, unit-cell.

## References:

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## 1. Transmitarray Operation Mode

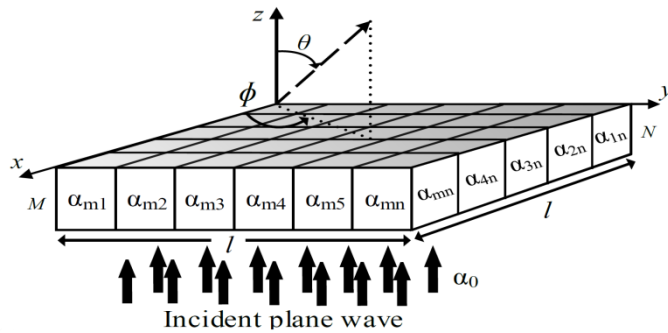


Figure 1: Proposed model for 2D beamsteering analysis.

$$\begin{cases} \psi_x = -\frac{2\pi}{\lambda} \cdot p \cdot \sin(\theta) \cdot \cos(\phi) \\ \psi_y = -\frac{2\pi}{\lambda} \cdot p \cdot \sin(\theta) \cdot \sin(\phi) \end{cases}, (1)$$

- When a planar incident electromagnetic wave propagates through the transmitarray, it experiences a different phase shifting, proportional to the elements transmission phase  $\alpha_{mn}$  as illustrated in Fig. 1.

- Due to the gradient phase distribution along both direction of the array, the re-transmitted wave direction ( $\theta$ ,  $\phi$ ) can be calculated using Eq. (1), where  $\psi_x$  and  $\psi_y$  are the progressive phase along the X and Y axis, respectively, and  $p$  is the periodicity of array elements.

- By changing the phase  $\alpha_{mn}$  of each array element in an progressive way, the original incident wave can be steered towards the desired output direction, relative to the normal of the structure.

## 2. Transmitarray Design, Simulation and Prototyping

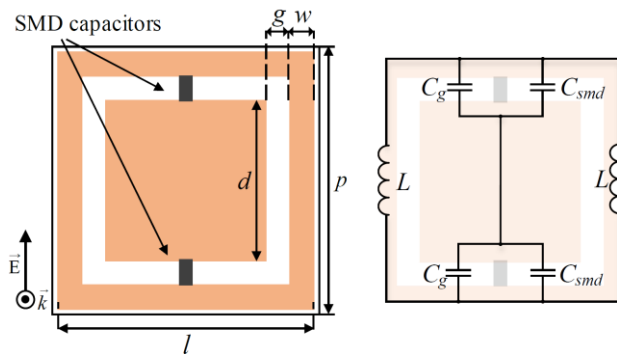


Figure 2: Square slot unit-cell and equivalent circuit.

**Dimensions:**  $p = 33 \text{ mm}$ ,  $l = 32.8 \text{ mm}$ ,  $d = 24 \text{ mm}$ ,  $g = 1.5 \text{ mm}$  and  $w = 3 \text{ mm}$ , using Nelco NX9250 substrate with thickness  $t = 1.5 \text{ mm}$ ,  $\epsilon_r = 2.50$ ,  $\tan\delta = 0.0017$ .

The square slot unit-cell, of Fig. 2, is proposed to reach phase ( $\alpha_{mn}$ ) control in each individual element of the array, and it counts with the following characteristics:

- **Spatial filtering:** EM wave passes through the structure with low insertion losses, Fig.3a;
- **Band-pass filtering characteristic** is shifted from 5 to 5.45 GHz when capacitance is modified from 2.8 to 0.7 pF;
- **Extended phase range**, up to  $360^\circ$  (Fig.3b), is achieved by stacking 5 layers of unit-cells at a distance of  $\lambda/16$ , separated by an air gap to increase the bandwidth and phase range;
- **Steering output range** up to  $\theta = 25^\circ$  and  $\phi = 25^\circ$  equivalent to  $A_z = 22^\circ$  and  $E_l = 10^\circ$  in Azimuth over Elevation coordinate system, when mounted as a 5 x 5 array.

## 2. Transmitarray Design, Simulation and Prototyping (cont.)

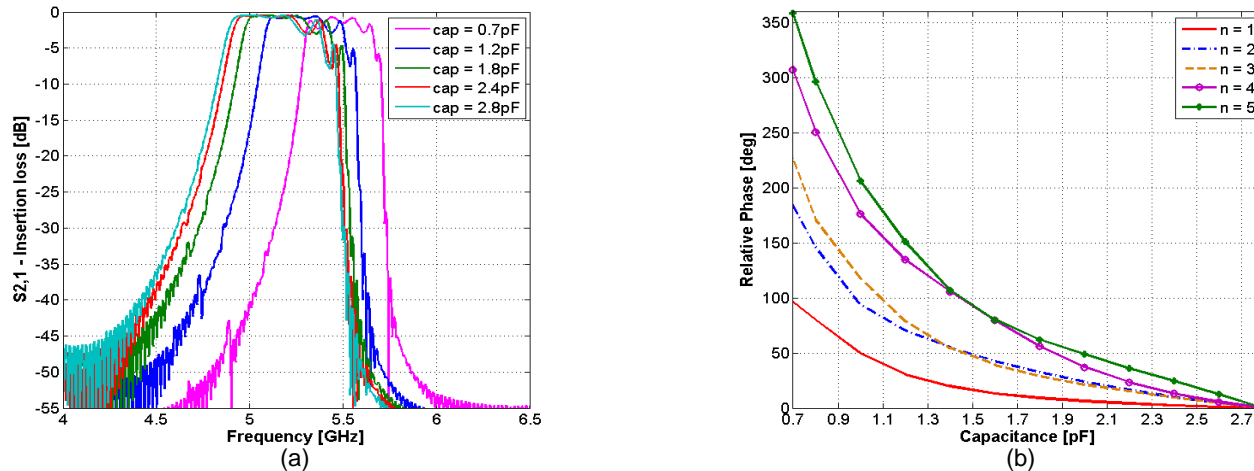


Figure 3: Simulated (a)  $S_{2,1}$  insertion loss (dB) and (b) Relative phase at 5.35GHz.

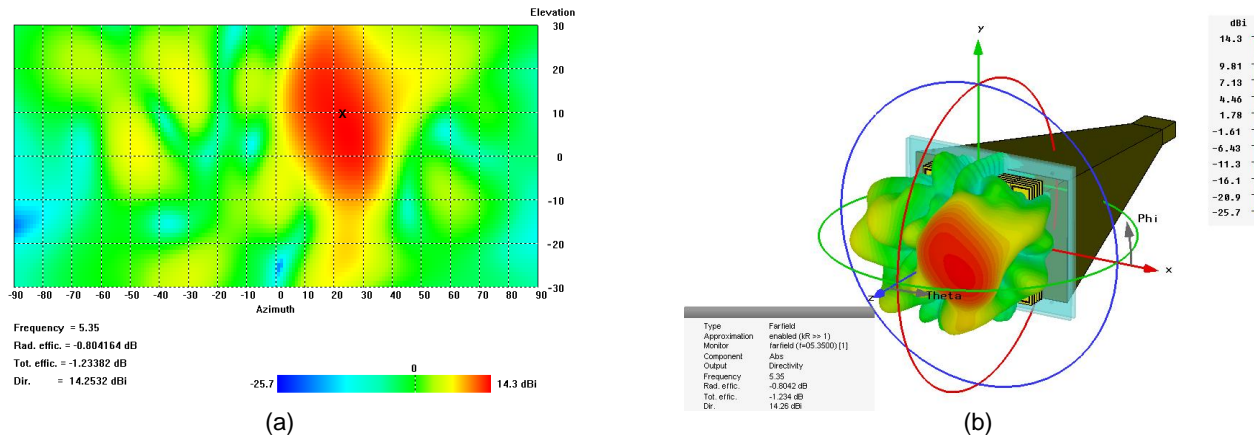
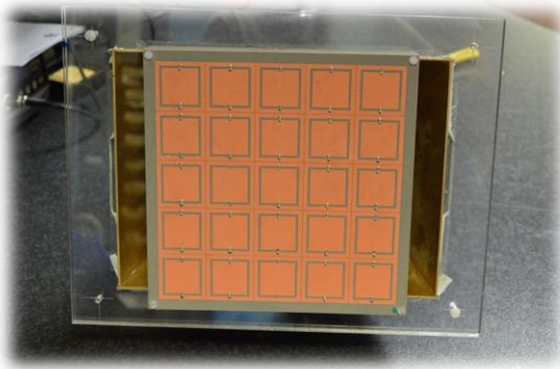


Figure 4: Simulated (a) 2D far-field plot and (b) 3D radiation pattern for  $Az = 22^\circ$  and  $El = 10^\circ$  ( $\theta = 25^\circ$ ,  $\phi = 25^\circ$ ), using the transmitarray in front of a realistic model of a 20dBi horn antenna.

## 3. Experimental Results

To assess the prototype performance, both **2D far-field plot** and **3D radiation pattern** are compared with a reference horn antenna. The antenna with the transmitarray, has the following specifications:

- A maximum directivity of  $11.4 \text{ dBi}$  at  $A_z = 20^\circ$  and  $E_l = 8^\circ$  ( $\theta = 22.5^\circ$ ,  $\phi = 21.5^\circ$ );
- HPBW of  $18^\circ$  in azimuth and  $21^\circ$  in elevation;
- Main lobe to side lobe level around 7dB.



(a)

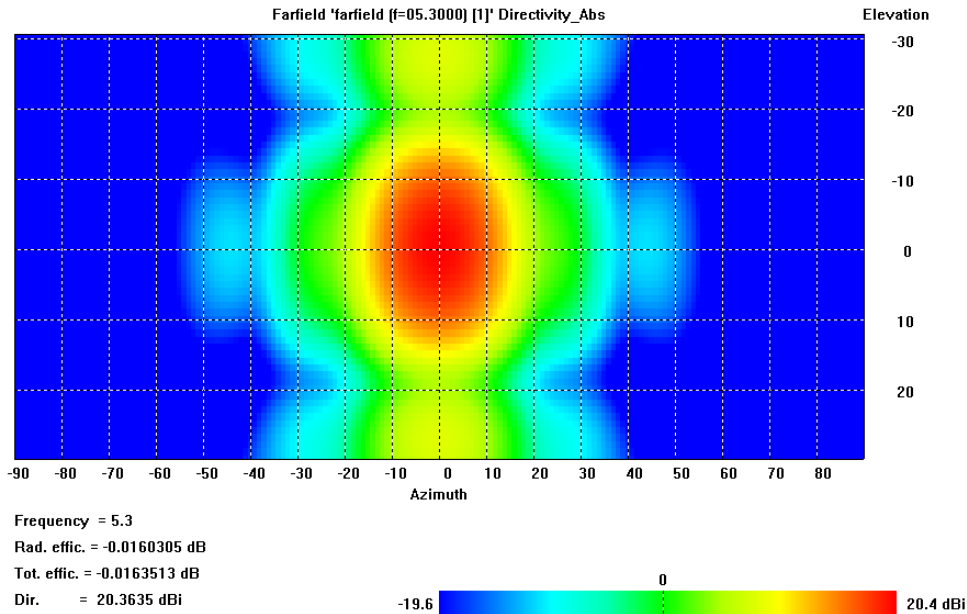


(b)

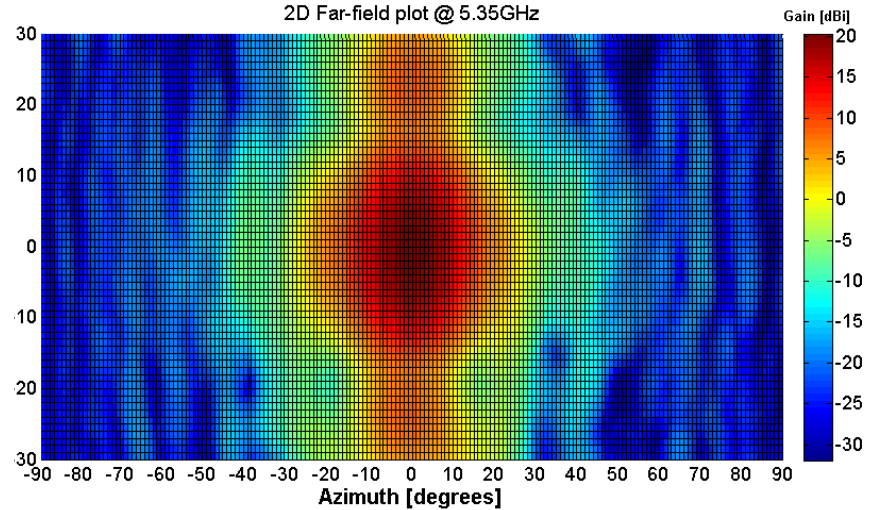
**Figure 5:** (a) Transmitarray prototype and (b) illustration of the setup inside the anechoic chamber for the 3D radiation pattern measurement.

## 3.1 Reference Radiation Pattern @5.35GHz *Antenna only (no MM structure)*

### Simulated Result



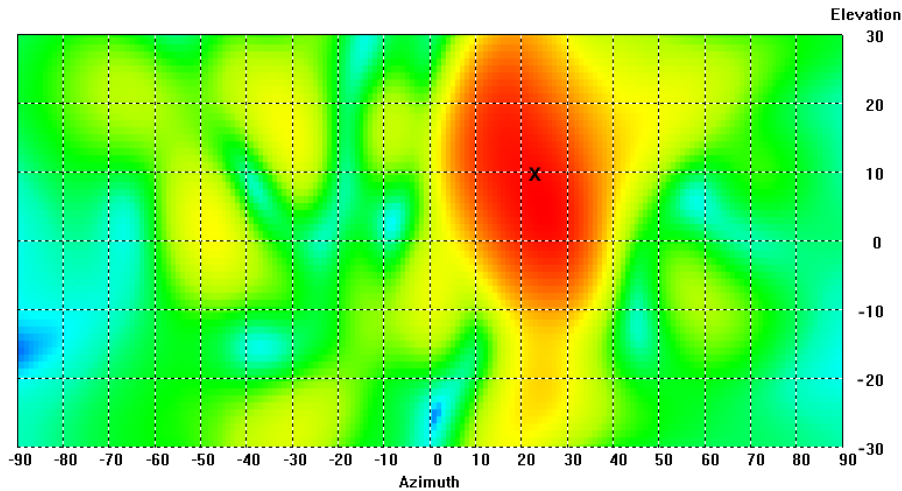
### Measurement Result



## 3.2 Desired Output Angle @ 5.35GHz

$$\theta = 25^\circ \text{ and } \phi = 25^\circ \gg Az = 22^\circ \text{ and } El = 10^\circ$$

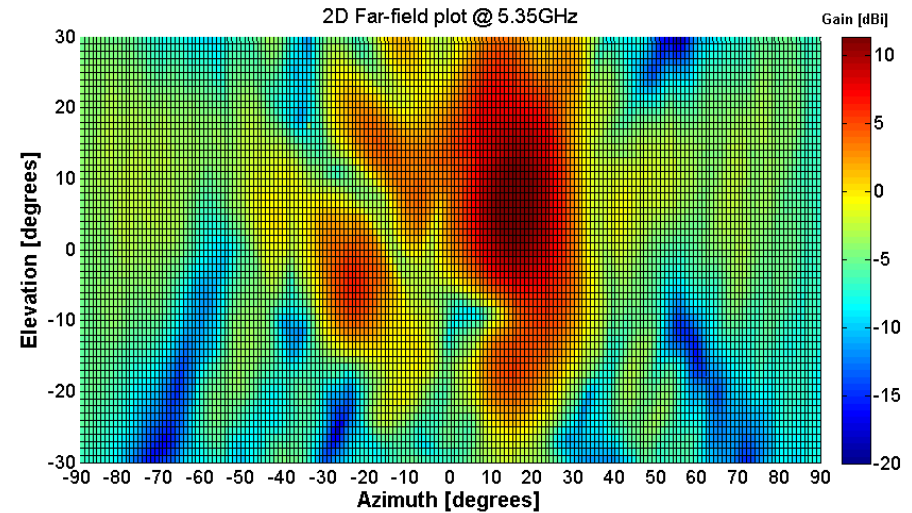
### Simulated Results



Frequency = 5.35  
Rad. effic. = -0.804164 dB  
Tot. effic. = -1.23382 dB  
Dir. = 14.2532 dBi



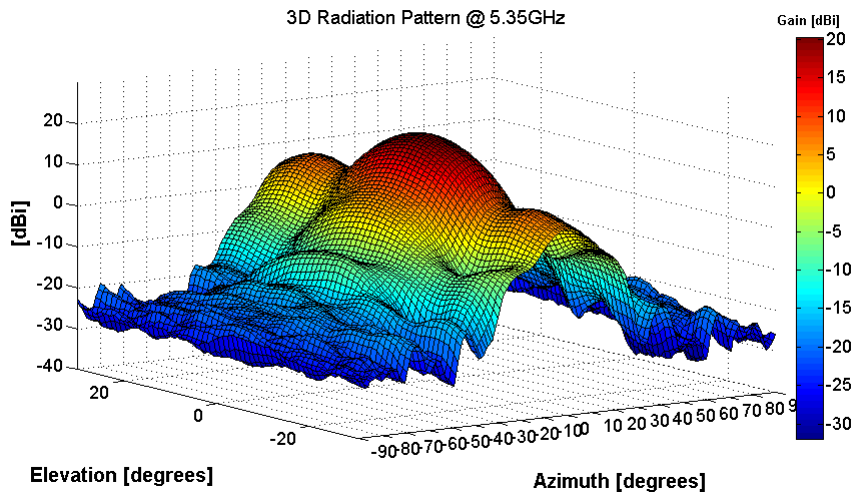
### Measurement Results



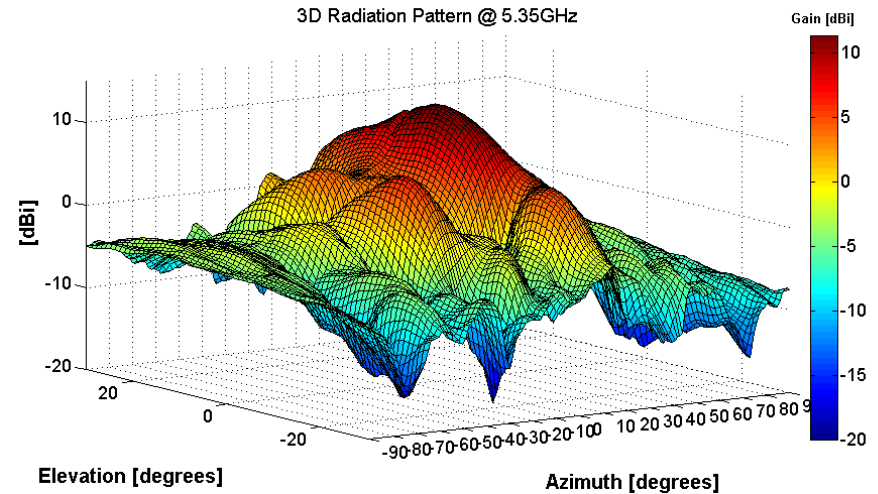
## 3.3 Desired Output Angle @ 5.35GHz

$$\theta = 25^\circ \text{ and } \phi = 25^\circ \gg Az = 22^\circ \text{ and } El = 10^\circ$$

**Measured  
Antenna only (original)**



**Measured  
Antenna w/ structure**





## Conclusions

A new approach to the analysis of a metamaterial based transmitarray with 2D-beamsteering capability is proposed and validated by means of EM simulations and measurements. It was successfully demonstrated that the radiation pattern of a horn antenna can be shifted towards  $\theta = 25^\circ$  and  $\phi = 25^\circ$  (  $A_z = 22^\circ$  and  $El = 10^\circ$  ), when the transmitarray is coupled to the aperture of the antenna.